

Method of precision increase by averaging with application to numerical differentiation

Andrej Liptaj*

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Abstract

If several independent algorithms for a computer-calculated quantity exist, then one can expect their results (which differ because of numerical errors) to follow approximately Gaussian distribution. The mean of this distribution, interpreted as the value of the quantity of interest, can be determined with better precision than what is the precision provided by a single algorithm. Often, with lack of enough independent algorithms, one can proceed differently: many practical algorithms introduce a bias using a parameter, e.g. a small but finite number to compute a limit or a large but finite number (cutoff) to approximate infinity. One may vary such parameter of a single algorithm and interpret the resulting numbers as generated by several algorithms. A numerical evidence for the validity of this approach is shown for differentiation.

1 Introduction

Average understood as summation (divided by a constant) is under very general assumptions subject to the central limit theorem. This can be used in numerical computations for precision increase. Indeed, if several independent

*Institute of Physics, Bratislava, Slovak Academy of Sciences, andrej.liptaj@savba.sk
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algorithms for computing a quantity of interest exist, each of them having certain numerical imprecision, one may average the results and get a smaller error. Depending on circumstances, this procedure may be regarded as repeated unbiased independent measurements with random errors and, for this scenario, the expected shrinking of the error is

$$\sigma = \frac{\sqrt{\sum_{i=1}^N \sigma_i^2}}{N} \approx \frac{\sigma^{typical}}{\sqrt{N}},$$

where one expects the numerical errors of the various methods not to be very different (all close to a typical value $\sigma^{typical}$).

The question of algorithm independence arises. Clearly, if each algorithm from a given set leads to the same result then the algorithms are, in the mathematical sense, fully correlated. However, for what concerns numerical errors, a different optics can be adopted: otherwise result-equivalent algorithms may differ a lot in the functions they use (and the corresponding register operations) which de-correlates their numerical uncertainties. It is reasonable to assume that the numerical errors arise from technical details of the computer processing and do not actually depend a lot on the global “idea” of a given algorithm. Therefore one can reasonably assume that algorithms which differ in “technical” sense provide practically uncorrelated numerical errors of their results.

Unfortunately, in practice, one usually does not have many independent methods to compute a given quantity. However what is often the case is a biased parameter-dependent algorithm. The parameters allow to approximate an ideal situation which is inaccessible via computers: a small (but finite) h can be used as a step in numerical differentiation or integration, a large (but finite) Λ can be used as a cutoff (approximating infinity). A natural idea arises: one may use different (but reasonable) values for these parameters, get in each case a result and apply the previous ideas. Two issues can be addressed here: bias and error correlations.

Obviously, any numerical differentiation (as an example) with nonzero step h is biased and even if infinite-precision computers were available the result would not be fully correct. The overall “wrongness” thus has two components: numerical errors and bias. Here an expectation can be made: if the averaging helps to shrink the numerical errors then one should tend to use, in the averaging approach, an algorithm (its parameter values) with smaller bias. In other words: the averaging cannot remove the bias but does

remove numerical effects and so one expects to get the most precise results for less biased algorithm compared to the bias leading to the most precise results for a single (i.e. non-averaged) algorithm.

The correlation of uncertainties of results from the parameter-changing approach is something one can examine empirically. The case of numerical differentiation studied in this text shows that their mutual independence is large enough to provide substantial error reduction.

In what follows, this text fully focuses on the numerical differentiation. To honestly study the subject I will use several methods of numerical differentiation. The corresponding issues will be reviewed in Sec. 2. Next, in Sec. 3, I will explain the heuristic testing method and present its results. In the last sections I will discuss different result-related observations and make summary and conclusions.

2 Numerical differentiation methods

In this text I focus on the (ill-conditioned) numerical differentiation of a general (differentiable) function, I will therefore ignore special recipes suited for special situations¹. To make sure that the error shrinking by averaging is not limited to some specific algorithm, I propose to test it on three different differentiation methods (with an appropriately chosen h):

- Averaged finite difference (AFD)

$$\begin{aligned} f'_{AFD}(x, h) &= \frac{1}{2} \left[\frac{f(x+h) - f(x)}{h} + \frac{f(x) - f(x-h)}{h} \right], \\ &= \frac{f(x+h) - f(x-h)}{2h}. \end{aligned}$$

- “Five-point rule” based on the Richardson extrapolation (RE)

$$f'_{RE}(x, h) = \frac{f(x-2h) - 8f(x-h) + 8f(x+h) - f(x+2h)}{12h}.$$

The implementation of the numerical differentiation is in many common mathematical computer packages based on the Richardson extrapolation.

¹E.g. the set of analytic functions and well-conditioned differentiation based on the Cauchy theorem.

- Lanczos differentiation by integration (LDI)

$$f'_{LDI}(x, h) = \frac{3}{2h^3} \int_{x-h}^{x+h} (x-t) f(t) dt.$$

To evaluate the integral I use, in my programs, the composite Boole's rule with 16 equidistant points $\{x_i\}_{i=1}^{i=16}$, $x_1 = x - h$, $x_{16} = x + h$, $x_{i+1} - x_i = \Delta x$

$$\int_{x-h}^{x+h} f(t) dt \approx 2 \Delta x (I_1 + I_2 + I_3 + I_4) / 45,$$

$$I_1 = 7 [f(x_1) + f(x_{16})],$$

$$I_2 = 32 \sum_{i=1}^{i=7} f(x_{2i+1}),$$

$$I_3 = 14 \sum_{i=1}^{i=3} f(x_{4i}),$$

$$I_4 = 12 \sum_{i=0}^{i=3} f(x_{4i+2}).$$

Let me index these methods by the letter k , $k \in \{\text{AFD}, \text{RE}, \text{LDI}\}$. I implement the averaging procedure in the straightforward way

$$f'_k{}^{AV}(x) = \frac{1}{N} \sum_{i=1}^N f'_k(x, h_i), \quad h_i \in H,$$

where the set H is chosen in function of the h used in the single algorithm computation as follows:

- For AFD $H = [0.5h, 1.5h]$ where two options are investigated
 - h_i is generated as a random number with uniform distribution from the interval H (noted AFD_{MC}^{AV}).
 - successive values of h_i are generated such as to be equidistant with $h_1 = 0.5h$ and $h_N = 1.5h$ (noted AFD_{ED}^{AV}).
- For RE and LDI $H = [0.5h, 1.5h]$, where h_i is generated as a random number with uniform distribution from this interval (only this option is investigated).

Use of random numbers seems to be a safer option if aiming uncorrelated errors, yet regular division of the interval is tested also. For testing purposes I use a program² written in the *JAVA* programming language and double precision variables.

3 Testing and results

To study the behavior of the method in more details I make an effort to examine it depending on the first and second derivatives of the function and on the step size h . The first quantity directly correlates with what is being approximated (f'), the two others (f'' , h) are often related to the expected precision of the approximation. I do the analysis by scanning 6 orders of magnitude for each “dependence” (its absolute value). For that purpose I choose 19 points in the $|f'|, |f''|$ plane, trying, in the logarithmic scale, to map it more or less uniformly. To avoid any fine-tuning suspicions I choose to use the basic elementary functions: $\cos(x)$, $\exp(x)$, $\ln(x)$ and $\arctan(x)$. However, with this choice, it is impossible to “uniformly” cover the $10^{-3} \lesssim |f'|, |f''| \lesssim 10^3$ region. Aiming this purpose, I add a suitable polynomial: the Laguerre polynomial $L_7(x)$. Situation is summarized in Tab 1 and in Fig. 1. From now on I will use the word “case” to refer to any of the 19 settings, each of them characterized by a function f , its argument x and the absolute value of its first and second derivatives at x . I will stick to the numbering presented in Tab. 1.

The step size h is changed from $h = 10^{-3}$ to $h = 10^{-8}$ in geometrical progression with factor 10. One needs also to define the size of the statistical sample. To profit most from the averaging method a big number is suitable; I fix it to $N = 10^6$. This choice is driven also by practical considerations, i.e. the wish to keep the computer processing time in reasonable limits (\sim minutes). The error is shown as absolute error

$$|f'_{\text{approximated}} - f'_{\text{true}}|, \tag{1}$$

where for f'_{true} the numerical value of the corresponding (known) derivative function is taken.

²The program can be, at least temporarily, downloaded from http://www.dthph.sav.sk/fileadmin/user_upload/liptaj/differentiationAveraging.zip or requested from the author. I also greatly profited from the WxMaxima software.

| Case number | Function | $x=$ | $ f'(x) \approx$ | $ f''(x) \approx$ |
|-------------|--------------|----------|-------------------|--------------------|
| 1 | $L_7(x)$ | 9.683 | 19.88 | 0.0011 |
| 2 | $L_7(x)$ | 11.2345 | 0.0031 | 28.57 |
| 3 | $L_7(x)$ | 15.83 | 265.1 | 0.1534 |
| 4 | $L_7(x)$ | 17.65 | 1.443 | 358.1 |
| 5 | $L_7(x)$ | 15.8285 | 265.1 | 0.0026 |
| 6 | $L_7(x)$ | 17.64595 | 0.0048 | 356.8 |
| 7 | $\exp(x)$ | -6.9 | 0.0010 | 0.0010 |
| 8 | $\ln(x)$ | 10 | 0.1 | 0.01 |
| 9 | $\arctan(x)$ | 6.245 | 0.0249 | 0.0078 |
| 10 | $\cos(x)$ | 1.47 | 0.9949 | 0.1006 |
| 11 | $\cos(x)$ | 0.1 | 0.0998 | 0.9950 |
| 12 | $\cos(x)$ | 0.0025 | 0.0024 | 0.9999 |
| 13 | $\arctan(x)$ | 0.002 | 0.9999 | 0.0039 |
| 14 | $\ln(x)$ | 0.03 | 33.33 | 1111.1 |
| 15 | $\exp(x)$ | 6.9 | 992.2 | 992.2 |
| 16 | $\ln(x)$ | 1.0 | 1.0 | 1.0 |
| 17 | $L_7(x)$ | 9.67477 | 19.88 | 0.1000 |
| 18 | $L_7(x)$ | 11.2311 | 0.1001 | 28.49 |
| 19 | $\exp(x)$ | 4.25 | 70.10 | 70.10 |

Table 1: Cases (points and functions) for which the averaging procedure was tested.

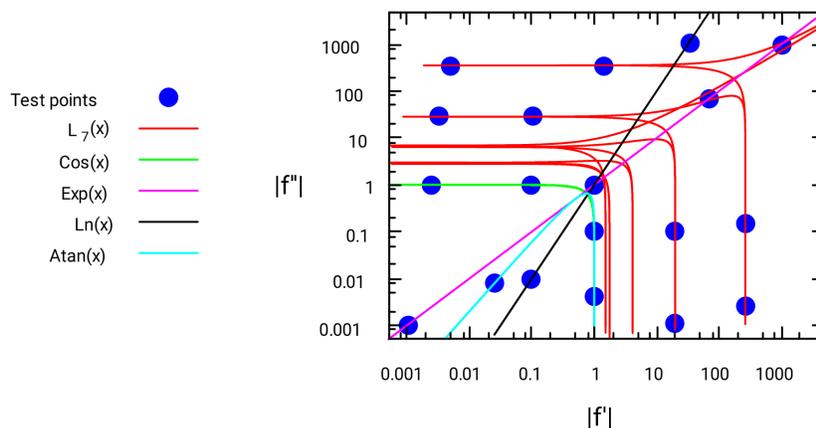


Figure 1: Studied cases depicted in $|f'|, |f''|$ the plane.

To prevent long listings within the main text, I put the tables with detailed results in Attachment. Each table corresponds to a single case and is differential in the step size and used method. Here, I average these tables (i.e. I average each cell over 19 cases), which might be somewhat artificial but has more message-conveying power.

| h | Case-averaged results | | |
|-----------------|--|---|--|
| | 10^{-3} | 10^{-4} | 10^{-5} |
| AFD | 2.0×10^{-3} | 2.0×10^{-5} | 1.8×10^{-7} |
| AFD_{MC}^{AV} | 2.2×10^{-3} | 2.2×10^{-5} | 2.2×10^{-7} |
| AFD_{ED}^{AV} | 1.2×10^{-3} | 1.2×10^{-5} | 1.2×10^{-7} |
| RE | 6.9×10^{-9} | 7.6×10^{-9} | 7.1×10^{-8} |
| RE^{AV} | 1.1×10^{-8} | 6.0×10^{-12} | 4.2×10^{-11} |
| LDI | 1.2×10^{-3} | 1.4×10^{-5} | 7.2×10^{-4} |
| LDI^{AV} | 1.3×10^{-3} | 1.3×10^{-5} | 4.4×10^{-7} |

| h | Case-averaged results | | |
|-----------------|--|--|----------------------|
| | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 3.0×10^{-7} | 1.8×10^{-6} | 6.3×10^{-2} |
| AFD_{MC}^{AV} | 2.3×10^{-9} | 3.1×10^{-9} | 5.1×10^{-5} |
| AFD_{ED}^{AV} | 1.7×10^{-9} | 1.6×10^{-9} | 1.0×10^{-6} |
| RE | 4.3×10^{-7} | 2.4×10^{-6} | 9.4×10^{-2} |
| RE^{AV} | 7.1×10^{-10} | 1.0×10^{-9} | 4.0×10^{-5} |
| LDI | 7.2×10^{-2} | 5.5×10^0 | 1.2×10^7 |
| LDI^{AV} | 9.3×10^{-5} | 5.1×10^{-3} | 8.0×10^3 |

4 Discussion

Results confirm that the averaging method is very efficient in providing precise numerical derivative and reducing related errors. The overall error reduction (in absolute error) typically corresponds to two or three orders of magnitude (when comparing the most precise results). Besides the obvious

fact of reducing the error by increasing statistics³, the assumptions concerning method functioning are further confirmed by the behavior with respect to h : as predicted earlier (Sec. 1) the most precise results of the averaging method typically happen for smaller step h than is h which corresponds to the most precise result of the same, but non-averaged method. Rather numerous are situations where h remains the same, rare are exceptions where the behavior is opposite (RE method in case 12 and AFD_{MC}^{AV} method in case 16). Rather amazing are results of the RE^{AV} method in cases 13 and 14 where, within the computer precision, exact results are reconstructed.

When comparing AFD_{MC}^{AV} and AFD_{ED}^{AV} approaches, one observes that their performances are rather equivalent. Yet, the “equidistant” method performs somewhat better which is little bit surprising: one can imagine that a regular division could introduce some correlation into the numbers to be averaged and thus slightly spoil the results. One can speculate that this behavior could be related to what is known from quasi-Monte Carlo methods: random numbers are often distributed quite unevenly, i.e. the “low-discrepancy” of the equidistant method may be the reason for it to win. It might certainly be a good idea for further studies to use, within the averaging method, low-discrepancy sequences.

The results also show that the averaging method can be combined with any of the three proposed “standard” methods, which points once more to the general statistical aspects of the method. One may notice that the “standard” methods differ quite not only in the definition but also in the optimal step size h (step where the maximal precision is reached). The most precise of them is clearly the one based on the Richardson extrapolation.

Finally, one needs to remark that for the LDI method in cases 14 and 16 the averaging method fails. I cannot think about a solid explanation, it might be a random accident or it might be somehow related to the fact of LDI being the least precise of the studied methods (or any other feature of this method). At least in the case 14 the non-averaged result is atypically precise for this method, which might be interpreted as a “luck”. In case 16 the difference between results is small, making the averaging failure not to be so “pronounced”. In any case I need to stress that, despite these two observations, the averaging method works in general very well also for the LDI algorithm.

³Non-averaged results can be seen as averaged results with statistics equal to one.

5 Summary and conclusion

In this text I made a numerical study of the averaging method applied to the numerical differentiation. A rigorous approach to the whole idea would require a rigorous treatment of the floating-point arithmetic in computer registers. If possible, such an approach would certainly be very tedious with many assumptions and special cases. I believe a numerical evidence is strong enough to make claims about the method and its mechanism. The method is efficient and provides an important precision increase. It is very general and robust because of its statistical character. It should be used in situations where precision is the priority, its main drawback, slowness, makes it not suitable for quick computations. When combined with a high precision “standard” method, the averaging method is, to my knowledge, the most precise numerical differentiation method at the market today.

Appendix

The following tables give detailed results for cases mentioned in Tab 1. In each table the step h is varied from 10^{-3} to 10^{-8} in columns, in rows different methods are presented (notation from Sec. 2 is used). Individual cells contain absolute error (formula 1), the most precise of them is, for each method, shown in bold characters.

| Case number: 1 | | | | | | |
|-----------------|---|---|--|---|-----------------------|----------------------|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 2.1×10^{-4} | 2.1×10^{-6} | 4.9×10^{-9} | 2.1×10^{-7} | 1.2×10^{-6} | 9.5×10^{-5} |
| AFD_{MC}^{AV} | 2.2×10^{-4} | 2.2×10^{-6} | 2.2×10^{-8} | 2.3×10^{-10} | 1.8×10^{-9} | 6.4×10^{-8} |
| AFD_{ED}^{AV} | 1.2×10^{-4} | 1.2×10^{-6} | 1.2×10^{-8} | 3.9×10^{-10} | 5.2×10^{-10} | 2.1×10^{-9} |
| RE | 1.5×10^{-10} | 4.4×10^{-10} | 2.3×10^{-8} | 2.9×10^{-7} | 1.9×10^{-6} | 1.5×10^{-4} |
| RE^{AV} | 5.0×10^{-11} | 1.7×10^{-12} | 1.2×10^{-11} | 2.9×10^{-10} | 7.8×10^{-11} | 9.4×10^{-8} |
| LDI | 1.2×10^{-4} | 8.4×10^{-7} | 2.6×10^{-5} | 2.6×10^{-3} | 1.3×10^{-1} | 2.6×10^4 |
| LDI^{AV} | 1.3×10^{-4} | 1.3×10^{-6} | 2.8×10^{-8} | 8.4×10^{-6} | 5.5×10^{-4} | 1.1×10^1 |

| Case number: 2 | | | | | | |
|-----------------|----------------------|---|--|---|-----------------------|----------------------|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 3.9×10^{-4} | 3.9×10^{-6} | 1.7×10^{-8} | 3.4×10^{-7} | 1.8×10^{-6} | 4.8×10^{-4} |
| AFD_{MC}^{AV} | 4.2×10^{-4} | 4.2×10^{-6} | 4.2×10^{-8} | 4.5×10^{-10} | 2.1×10^{-9} | 4.7×10^{-7} |
| AFD_{ED}^{AV} | 2.3×10^{-4} | 2.3×10^{-6} | 2.3×10^{-8} | 4.0×10^{-10} | 6.0×10^{-10} | 1.8×10^{-9} |
| RE | 2.2×10^{-9} | 4.4×10^{-10} | 3.0×10^{-8} | 4.1×10^{-7} | 2.2×10^{-6} | 7.2×10^{-4} |
| RE^{AV} | 2.8×10^{-9} | 7.0×10^{-12} | 9.5×10^{-12} | 4.8×10^{-10} | 2.8×10^{-9} | 2.7×10^{-7} |
| LDI | 2.3×10^{-4} | 1.6×10^{-6} | 4.9×10^{-5} | 4.9×10^{-3} | 2.4×10^{-1} | 1.2×10^5 |
| LDI^{AV} | 2.5×10^{-4} | 2.5×10^{-6} | 1.4×10^{-7} | 5.5×10^{-6} | 4.9×10^{-4} | 2.6×10^0 |

| Case number: 3 | | | | | | |
|-----------------|----------------------|---|--|--|----------------------|----------------------|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 1.7×10^{-3} | 1.7×10^{-5} | 9.6×10^{-8} | 2.5×10^{-7} | 1.1×10^{-6} | 4.6×10^{-2} |
| AFD_{MC}^{AV} | 1.8×10^{-3} | 1.8×10^{-5} | 1.8×10^{-7} | 1.3×10^{-9} | 2.3×10^{-8} | 2.2×10^{-5} |
| AFD_{ED}^{AV} | 9.8×10^{-4} | 9.8×10^{-6} | 9.8×10^{-8} | 5.5×10^{-9} | 1.4×10^{-8} | 7.4×10^{-7} |
| RE | 1.1×10^{-8} | 6.3×10^{-9} | 1.0×10^{-7} | 4.8×10^{-7} | 5.1×10^{-7} | 6.9×10^{-2} |
| RE^{AV} | 1.8×10^{-8} | 2.0×10^{-11} | 1.2×10^{-10} | 4.1×10^{-9} | 1.9×10^{-9} | 6.4×10^{-5} |
| LDI | 1.0×10^{-3} | 1.1×10^{-6} | 6.0×10^{-4} | 6.0×10^{-2} | 3.0×10^0 | 1.2×10^7 |
| LDI^{AV} | 1.1×10^{-3} | 1.1×10^{-5} | 6.2×10^{-7} | 4.6×10^{-5} | 6.5×10^{-3} | 1.0×10^4 |

| Case number: 4 | | | | | | |
|-----------------|--|---|--|---|-----------------------|----------------------|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 5.3×10^{-3} | 5.3×10^{-5} | 1.1×10^{-7} | 2.6×10^{-6} | 1.9×10^{-5} | 5.4×10^{-1} |
| AFD_{MC}^{AV} | 5.7×10^{-3} | 5.7×10^{-5} | 5.7×10^{-7} | 4.9×10^{-9} | 1.7×10^{-8} | 6.3×10^{-4} |
| AFD_{ED}^{AV} | 3.1×10^{-3} | 3.1×10^{-5} | 3.1×10^{-7} | 2.3×10^{-10} | 9.7×10^{-10} | 9.0×10^{-6} |
| RE | 2.1×10^{-8} | 8.7×10^{-8} | 6.2×10^{-7} | 3.8×10^{-6} | 2.7×10^{-5} | 8.0×10^{-1} |
| RE^{AV} | 2.7×10^{-8} | 1.8×10^{-11} | 3.4×10^{-10} | 1.7×10^{-9} | 4.0×10^{-9} | 5.7×10^{-5} |
| LDI | 3.2×10^{-3} | 2.2×10^{-5} | 9.6×10^{-4} | 9.6×10^{-2} | 9.6×10^0 | 9.9×10^7 |
| LDI^{AV} | 3.4×10^{-3} | 3.4×10^{-5} | 1.7×10^{-6} | 7.1×10^{-4} | 1.9×10^{-2} | 6.5×10^4 |

| Case number: 5 | | | | | | |
|-----------------|----------------------|---|--|--|----------------------|----------------------|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 1.7×10^{-3} | 1.7×10^{-5} | 5.2×10^{-8} | 2.1×10^{-7} | 5.8×10^{-6} | 4.7×10^{-2} |
| AFD_{MC}^{AV} | 1.8×10^{-3} | 1.8×10^{-5} | 1.8×10^{-7} | 2.2×10^{-9} | 6.7×10^{-9} | 6.0×10^{-5} |
| AFD_{ED}^{AV} | 9.8×10^{-4} | 9.8×10^{-6} | 9.8×10^{-8} | 2.4×10^{-9} | 5.7×10^{-9} | 1.4×10^{-7} |
| RE | 9.2×10^{-9} | 7.9×10^{-9} | 1.6×10^{-7} | 4.5×10^{-7} | 5.9×10^{-6} | 6.9×10^{-2} |
| RE^{AV} | 1.8×10^{-8} | 1.9×10^{-11} | 3.3×10^{-11} | 1.3×10^{-9} | 4.3×10^{-9} | 3.1×10^{-5} |
| LDI | 1.0×10^{-3} | 1.1×10^{-6} | 6.0×10^{-4} | 6.0×10^{-2} | 3.0×10^0 | 1.2×10^7 |
| LDI^{AV} | 1.1×10^{-3} | 1.1×10^{-5} | 2.0×10^{-7} | 3.5×10^{-5} | 2.2×10^{-3} | 1.0×10^4 |

| Case number: 6 | | | | | | |
|-----------------|--|---|--|----------------------|--|----------------------|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 5.3×10^{-3} | 5.3×10^{-5} | 7.7×10^{-7} | 1.5×10^{-6} | 1.6×10^{-6} | 5.6×10^{-1} |
| AFD_{MC}^{AV} | 5.7×10^{-3} | 5.7×10^{-5} | 5.7×10^{-7} | 7.4×10^{-9} | 2.2×10^{-9} | 2.7×10^{-4} |
| AFD_{ED}^{AV} | 3.1×10^{-3} | 3.1×10^{-5} | 3.1×10^{-7} | 8.9×10^{-9} | 5.7×10^{-9} | 8.9×10^{-6} |
| RE | 1.7×10^{-8} | 3.3×10^{-8} | 3.3×10^{-7} | 1.9×10^{-6} | 2.0×10^{-6} | 8.4×10^{-1} |
| RE^{AV} | 2.7×10^{-8} | 3.0×10^{-11} | 2.1×10^{-10} | 4.8×10^{-9} | 1.2×10^{-9} | 6.0×10^{-4} |
| LDI | 3.2×10^{-3} | 2.2×10^{-5} | 9.6×10^{-4} | 9.6×10^{-2} | 9.6×10^0 | 9.8×10^7 |
| LDI^{AV} | 3.4×10^{-3} | 3.4×10^{-5} | 2.0×10^{-6} | 2.8×10^{-4} | 6.2×10^{-2} | 6.7×10^4 |

| Case number: 7 | | | | | | |
|-----------------|----------------------|--|-----------------------|-----------------------|-----------------------|---|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 2.1×10^{-2} | 2.1×10^{-4} | 2.1×10^{-6} | 2.5×10^{-7} | 1.1×10^{-7} | 3.7×10^{-12} |
| AFD_{MC}^{AV} | 2.3×10^{-2} | 2.3×10^{-4} | 2.3×10^{-6} | 2.2×10^{-8} | 6.6×10^{-10} | 5.0×10^{-15} |
| AFD_{ED}^{AV} | 1.2×10^{-2} | 1.2×10^{-4} | 1.2×10^{-6} | 1.2×10^{-8} | 9.6×10^{-10} | 6.2×10^{-17} |
| RE | 3.1×10^{-8} | 4.0×10^{-9} | 2.4×10^{-8} | 4.0×10^{-7} | 8.0×10^{-7} | 5.6×10^{-12} |
| RE^{AV} | 4.7×10^{-8} | 2.7×10^{-12} | 1.5×10^{-11} | 2.8×10^{-10} | 1.8×10^{-9} | 4.2×10^{-15} |
| LDI | 1.3×10^{-2} | 2.0×10^{-4} | 1.0×10^{-2} | 1.0×10^0 | 7.8×10^1 | 2.7×10^{-4} |
| LDI^{AV} | 1.4×10^{-2} | 1.4×10^{-4} | 3.5×10^{-6} | 6.5×10^{-4} | 4.0×10^{-3} | 3.3×10^{-7} |

| Case number: 8 | | | | | | |
|-----------------|---|---|--|---|-----------------------|-----------------------|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 2.5×10^{-4} | 2.5×10^{-6} | 4.8×10^{-8} | 2.2×10^{-7} | 7.6×10^{-8} | 1.3×10^{-4} |
| AFD_{MC}^{AV} | 2.7×10^{-4} | 2.7×10^{-6} | 2.7×10^{-8} | 2.4×10^{-10} | 1.3×10^{-9} | 7.7×10^{-8} |
| AFD_{ED}^{AV} | 1.5×10^{-4} | 1.5×10^{-6} | 1.5×10^{-8} | 7.2×10^{-11} | 8.6×10^{-11} | 3.7×10^{-10} |
| RE | 2.7×10^{-10} | 5.1×10^{-10} | 2.7×10^{-8} | 3.1×10^{-7} | 1.6×10^{-7} | 1.9×10^{-4} |
| RE^{AV} | 5.0×10^{-10} | 2.0×10^{-12} | 1.2×10^{-11} | 2.6×10^{-11} | 4.2×10^{-10} | 1.4×10^{-7} |
| LDI | 1.5×10^{-4} | 1.0×10^{-6} | 3.3×10^{-5} | 3.3×10^{-3} | 1.6×10^{-1} | 3.5×10^4 |
| LDI^{AV} | 1.6×10^{-4} | 1.6×10^{-6} | 6.9×10^{-8} | 8.7×10^{-6} | 7.1×10^{-4} | 1.7×10^1 |

| Case number: 9 | | | | | | |
|-----------------|----------------------|---|---|---|-----------------------|-----------------------|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 8.6×10^{-5} | 8.6×10^{-7} | 8.5×10^{-9} | 3.0×10^{-9} | 2.7×10^{-8} | 1.3×10^{-6} |
| AFD_{MC}^{AV} | 9.3×10^{-5} | 9.3×10^{-7} | 9.3×10^{-9} | 7.0×10^{-11} | 1.1×10^{-10} | 3.8×10^{-10} |
| AFD_{ED}^{AV} | 5.0×10^{-5} | 5.0×10^{-7} | 5.0×10^{-9} | 3.3×10^{-11} | 4.3×10^{-11} | 1.3×10^{-10} |
| RE | 1.1×10^{-9} | 7.6×10^{-11} | 2.0×10^{-10} | 6.2×10^{-9} | 4.2×10^{-8} | 1.7×10^{-6} |
| RE^{AV} | 1.6×10^{-9} | 1.9×10^{-13} | 1.9×10^{-13} | 2.2×10^{-11} | 1.7×10^{-10} | 1.3×10^{-9} |
| LDI | 5.2×10^{-5} | 5.6×10^{-7} | 5.5×10^{-6} | 5.5×10^{-4} | 4.1×10^{-2} | 1.4×10^2 |
| LDI^{AV} | 5.6×10^{-5} | 5.6×10^{-7} | 7.1×10^{-9} | 2.8×10^{-7} | 1.3×10^{-6} | 6.7×10^{-1} |

| Case number: 10 | | | | | | |
|-----------------|----------------------|---|---|---|---|-----------------------|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 4.5×10^{-5} | 4.5×10^{-7} | 4.5×10^{-9} | 1.1×10^{-10} | 6.7×10^{-10} | 1.4×10^{-10} |
| AFD_{MC}^{AV} | 4.9×10^{-5} | 4.9×10^{-7} | 4.9×10^{-9} | 4.9×10^{-11} | 2.6×10^{-12} | 6.1×10^{-12} |
| AFD_{ED}^{AV} | 2.7×10^{-5} | 2.7×10^{-7} | 2.7×10^{-9} | 2.7×10^{-11} | 1.8×10^{-13} | 2.9×10^{-13} |
| RE | 3.9×10^{-9} | 4.0×10^{-12} | 4.1×10^{-12} | 2.1×10^{-10} | 1.4×10^{-9} | 6.0×10^{-10} |
| RE^{AV} | 5.9×10^{-9} | 5.8×10^{-13} | 1.7×10^{-14} | 2.5×10^{-13} | 2.0×10^{-12} | 1.2×10^{-12} |
| LDI | 2.7×10^{-5} | 2.7×10^{-7} | 4.1×10^{-8} | 7.6×10^{-6} | 1.1×10^{-3} | 8.7×10^{-1} |
| LDI^{AV} | 3.0×10^{-5} | 3.0×10^{-7} | 2.7×10^{-9} | 2.6×10^{-8} | 1.7×10^{-6} | 1.0×10^{-3} |

| Case number: 11 | | | | | | |
|-----------------|----------------------|-----------------------|---|---|-----------------------|---|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 5.3×10^{-4} | 5.3×10^{-6} | 5.3×10^{-8} | 5.2×10^{-10} | 6.6×10^{-11} | 3.9×10^{-11} |
| AFD_{MC}^{AV} | 5.7×10^{-4} | 5.7×10^{-6} | 5.7×10^{-8} | 5.7×10^{-10} | 5.7×10^{-12} | 3.6×10^{-13} |
| AFD_{ED}^{AV} | 3.1×10^{-4} | 3.1×10^{-6} | 3.1×10^{-8} | 3.1×10^{-10} | 3.1×10^{-12} | 5.1×10^{-15} |
| RE | 6.8×10^{-9} | 7.0×10^{-13} | 5.8×10^{-13} | 2.2×10^{-12} | 6.6×10^{-11} | 4.1×10^{-10} |
| RE^{AV} | 1.0×10^{-8} | 1.0×10^{-12} | 8.9×10^{-16} | 3.6×10^{-15} | 4.5×10^{-14} | 1.4×10^{-13} |
| LDI | 3.2×10^{-4} | 3.2×10^{-6} | 3.3×10^{-8} | 5.0×10^{-7} | 3.3×10^{-5} | 1.8×10^{-2} |
| LDI^{AV} | 3.4×10^{-4} | 3.4×10^{-6} | 3.4×10^{-8} | 2.2×10^{-10} | 3.7×10^{-8} | 3.6×10^{-6} |

| Case number: 12 | | | | | | |
|-----------------|----------------------|-----------------------|---|---|---|---|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 5.8×10^{-4} | 5.8×10^{-6} | 5.8×10^{-8} | 5.8×10^{-10} | 7.8×10^{-12} | 4.3×10^{-10} |
| AFD_{MC}^{AV} | 6.3×10^{-4} | 6.3×10^{-6} | 6.3×10^{-8} | 6.3×10^{-10} | 6.3×10^{-12} | 2.8×10^{-13} |
| AFD_{ED}^{AV} | 3.4×10^{-4} | 3.4×10^{-6} | 3.4×10^{-8} | 3.4×10^{-10} | 3.4×10^{-12} | 8.0×10^{-14} |
| RE | 7.0×10^{-9} | 7.6×10^{-13} | 5.4×10^{-13} | 4.8×10^{-13} | 4.5×10^{-11} | 6.1×10^{-10} |
| RE^{AV} | 1.1×10^{-8} | 1.1×10^{-12} | 1.8×10^{-15} | 5.3×10^{-15} | 9.8×10^{-15} | 7.0×10^{-13} |
| LDI | 3.5×10^{-4} | 3.5×10^{-6} | 3.5×10^{-8} | 1.3×10^{-8} | 2.6×10^{-6} | 1.3×10^{-4} |
| LDI^{AV} | 3.8×10^{-4} | 3.8×10^{-6} | 3.8×10^{-8} | 4.3×10^{-10} | 4.4×10^{-9} | 3.8×10^{-7} |

| Case number: 13 | | | | | | |
|-----------------|----------------------|-----------------------|---|---|-----------------------|---|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 5.8×10^{-4} | 5.8×10^{-6} | 5.8×10^{-8} | 5.8×10^{-10} | 8.6×10^{-11} | 3.7×10^{-11} |
| AFD_{MC}^{AV} | 6.3×10^{-4} | 6.3×10^{-6} | 6.3×10^{-8} | 6.3×10^{-10} | 6.4×10^{-12} | 7.6×10^{-13} |
| AFD_{ED}^{AV} | 3.4×10^{-4} | 3.4×10^{-6} | 3.4×10^{-8} | 3.4×10^{-10} | 3.4×10^{-12} | 4.3×10^{-14} |
| RE | 7.0×10^{-9} | 7.1×10^{-13} | 2.7×10^{-13} | 8.4×10^{-13} | 7.7×10^{-11} | 2.2×10^{-10} |
| RE^{AV} | 1.1×10^{-8} | 1.1×10^{-12} | 0.0×10^0 | 1.3×10^{-14} | 3.8×10^{-14} | 7.7×10^{-14} |
| LDI | 3.5×10^{-4} | 3.5×10^{-6} | 3.5×10^{-8} | 1.3×10^{-8} | 2.6×10^{-6} | 1.3×10^{-4} |
| LDI^{AV} | 3.8×10^{-4} | 3.8×10^{-6} | 3.8×10^{-8} | 3.9×10^{-10} | 2.1×10^{-9} | 7.2×10^{-7} |

| Case number: 14 | | | | | | |
|-----------------|----------------------|-----------------------|---|---|---|---|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 5.7×10^{-4} | 5.7×10^{-6} | 5.7×10^{-8} | 5.6×10^{-10} | 1.9×10^{-11} | 3.0×10^{-11} |
| AFD_{MC}^{AV} | 6.1×10^{-4} | 6.1×10^{-6} | 6.1×10^{-8} | 6.1×10^{-10} | 6.2×10^{-12} | 5.1×10^{-13} |
| AFD_{ED}^{AV} | 3.3×10^{-4} | 3.3×10^{-6} | 3.3×10^{-8} | 3.3×10^{-10} | 3.3×10^{-12} | 4.9×10^{-14} |
| RE | 6.9×10^{-9} | 6.3×10^{-13} | 2.5×10^{-14} | 3.5×10^{-12} | 1.0×10^{-11} | 3.0×10^{-11} |
| RE^{AV} | 1.0×10^{-8} | 1.0×10^{-12} | 0.0×10^0 | 2.7×10^{-15} | 2.7×10^{-14} | 1.2×10^{-12} |
| LDI | 3.4×10^{-4} | 3.4×10^{-6} | 3.6×10^{-8} | 2.5×10^{-7} | 2.0×10^{-11} | 1.1×10^{-3} |
| LDI^{AV} | 3.7×10^{-4} | 3.7×10^{-6} | 3.7×10^{-8} | 2.1×10^{-10} | 6.2×10^{-9} | 4.8×10^{-6} |

| Case number: 15 | | | | | | |
|-----------------|----------------------|---|---|---|-----------------------|---|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 7.7×10^{-5} | 7.7×10^{-7} | 4.9×10^{-9} | 3.1×10^{-9} | 1.0×10^{-7} | 2.6×10^{-6} |
| AFD_{MC}^{AV} | 8.3×10^{-5} | 8.3×10^{-7} | 8.3×10^{-9} | 4.7×10^{-11} | 7.6×10^{-11} | 3.6×10^{-9} |
| AFD_{ED}^{AV} | 4.5×10^{-5} | 4.5×10^{-7} | 4.5×10^{-9} | 6.5×10^{-11} | 2.1×10^{-10} | 6.5×10^{-11} |
| RE | 1.1×10^{-9} | 2.2×10^{-10} | 4.1×10^{-9} | 4.5×10^{-9} | 9.9×10^{-8} | 3.9×10^{-6} |
| RE^{AV} | 1.8×10^{-9} | 3.8×10^{-13} | 1.6×10^{-12} | 9.6×10^{-12} | 4.8×10^{-10} | 1.4×10^{-9} |
| LDI | 4.6×10^{-5} | 5.1×10^{-7} | 6.7×10^{-6} | 6.7×10^{-4} | 5.1×10^{-2} | 2.6×10^2 |
| LDI^{AV} | 5.0×10^{-5} | 5.0×10^{-7} | 8.6×10^{-10} | 3.7×10^{-7} | 2.8×10^{-5} | 1.1×10^0 |

| Case number: 16 | | | | | | |
|-----------------|----------------------|---|---|-----------------------|---|---|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 1.6×10^{-4} | 1.6×10^{-6} | 1.6×10^{-8} | 1.3×10^{-10} | 1.2×10^{-10} | 5.9×10^{-11} |
| AFD_{MC}^{AV} | 1.7×10^{-4} | 1.7×10^{-6} | 1.7×10^{-8} | 1.7×10^{-10} | 6.7×10^{-13} | 1.4×10^{-12} |
| AFD_{ED}^{AV} | 9.1×10^{-5} | 9.1×10^{-7} | 9.1×10^{-9} | 9.1×10^{-11} | 1.1×10^{-12} | 2.4×10^{-13} |
| RE | 4.8×10^{-9} | 1.1×10^{-12} | 5.8×10^{-12} | 3.8×10^{-11} | 3.0×10^{-10} | 1.2×10^{-9} |
| RE^{AV} | 7.3×10^{-9} | 7.3×10^{-13} | 1.8×10^{-14} | 1.2×10^{-13} | 2.8×10^{-13} | 1.1×10^{-13} |
| LDI | 9.4×10^{-5} | 9.4×10^{-7} | 6.7×10^{-9} | 3.4×10^{-7} | 2.0×10^{-5} | 4.4×10^{-2} |
| LDI^{AV} | 1.0×10^{-4} | 1.0×10^{-6} | 9.9×10^{-9} | 2.3×10^{-8} | 2.4×10^{-6} | 1.6×10^{-2} |

| Case number: 17 | | | | | | |
|-----------------|---|---|--|---|-----------------------|-----------------------|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 2.0×10^{-4} | 2.0×10^{-6} | 2.7×10^{-8} | 1.8×10^{-8} | 2.0×10^{-6} | 1.0×10^{-4} |
| AFD_{MC}^{AV} | 2.2×10^{-4} | 2.2×10^{-6} | 2.2×10^{-8} | 2.4×10^{-10} | 1.2×10^{-9} | 6.9×10^{-10} |
| AFD_{ED}^{AV} | 1.2×10^{-4} | 1.2×10^{-6} | 1.2×10^{-8} | 1.3×10^{-10} | 2.5×10^{-10} | 5.1×10^{-7} |
| RE | 1.8×10^{-10} | 7.8×10^{-10} | 1.0×10^{-8} | 3.0×10^{-8} | 2.2×10^{-6} | 1.4×10^{-4} |
| RE^{AV} | 3.9×10^{-11} | 1.3×10^{-12} | 2.2×10^{-11} | 2.8×10^{-10} | 2.2×10^{-9} | 6.7×10^{-8} |
| LDI | 1.2×10^{-4} | 8.3×10^{-7} | 2.6×10^{-5} | 2.6×10^{-3} | 1.3×10^{-1} | 2.5×10^4 |
| LDI^{AV} | 1.3×10^{-4} | 1.3×10^{-6} | 1.7×10^{-8} | 2.7×10^{-7} | 1.2×10^{-4} | 3.6×10^1 |

| Case number: 18 | | | | | | |
|-----------------|--|---|--|---|-----------------------|----------------------|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 3.9×10^{-4} | 3.9×10^{-6} | 2.9×10^{-8} | 2.6×10^{-8} | 1.4×10^{-6} | 4.8×10^{-4} |
| AFD_{MC}^{AV} | 4.2×10^{-4} | 4.2×10^{-6} | 4.2×10^{-8} | 8.5×10^{-10} | 2.5×10^{-9} | 7.0×10^{-7} |
| AFD_{ED}^{AV} | 2.3×10^{-4} | 2.3×10^{-6} | 2.3×10^{-8} | 1.6×10^{-10} | 2.4×10^{-9} | 9.8×10^{-9} |
| RE | 1.8×10^{-9} | 3.2×10^{-9} | 1.7×10^{-8} | 6.3×10^{-8} | 1.9×10^{-6} | 6.8×10^{-4} |
| RE^{AV} | 2.7×10^{-9} | 7.1×10^{-12} | 3.4×10^{-11} | 1.4×10^{-10} | 8.6×10^{-11} | 1.1×10^{-6} |
| LDI | 2.3×10^{-4} | 1.6×10^{-6} | 4.9×10^{-5} | 4.9×10^{-3} | 2.4×10^{-1} | 1.2×10^5 |
| LDI^{AV} | 2.5×10^{-4} | 2.5×10^{-6} | 3.7×10^{-8} | 1.6×10^{-5} | 3.0×10^{-5} | 2.1×10^2 |

| Case number: 19 | | | | | | |
|-----------------|-----------------------|---|---|---|-----------------------|---|
| h | 10^{-3} | 10^{-4} | 10^{-5} | 10^{-6} | 10^{-7} | 10^{-8} |
| AFD | 1.0×10^{-6} | 1.0×10^{-8} | 7.6×10^{-10} | 2.7×10^{-9} | 1.6×10^{-8} | 1.9×10^{-7} |
| AFD_{MC}^{AV} | 1.1×10^{-6} | 1.1×10^{-8} | 1.1×10^{-10} | 1.5×10^{-12} | 5.7×10^{-11} | 2.2×10^{-10} |
| AFD_{ED}^{AV} | 5.8×10^{-7} | 5.8×10^{-9} | 5.8×10^{-11} | 3.8×10^{-12} | 2.9×10^{-11} | 3.0×10^{-12} |
| RE | 9.0×10^{-11} | 6.3×10^{-11} | 8.2×10^{-10} | 3.6×10^{-9} | 1.8×10^{-8} | 2.8×10^{-7} |
| RE^{AV} | 1.4×10^{-10} | 4.3×10^{-14} | 8.0×10^{-13} | 1.3×10^{-12} | 4.2×10^{-11} | 2.2×10^{-10} |
| LDI | 6.0×10^{-7} | 1.7×10^{-8} | 1.5×10^{-6} | 1.5×10^{-4} | 1.1×10^{-2} | 1.9×10^1 |
| LDI^{AV} | 6.5×10^{-7} | 6.5×10^{-9} | 4.1×10^{-10} | 4.1×10^{-8} | 1.3×10^{-5} | 8.0×10^{-2} |