

$$(r_1^{j_1 \dots j_n}(q), \dots, r_n^{j_1 \dots j_n}(q)) \leftrightarrow (p_1^{j_1}, \dots, p_n^{j_n}, q)$$

earlier established.

It is easy to observe that the set of functions (10) verifies the conditions (6) and thus they are a solution of the problem we had to solve.

Remarks: 1) The studied problem can be solved through other interpolation schemes as well.

2) It should be noted that these interpolation schemes are more precise as the number of the test inputs $p_1^{j_1}, \dots, p_n^{j_n}$, $0 \leq j_1 \leq m_1, \dots, 0 \leq j_n \leq m_n$, used to identify the system Σ , is greater.

3) Between two different interpolation schemes (but which use the same test inputs) it cannot be decided a priori which is better, as this depends on the particular nature of the system Σ .

4) The approximation method of the system Σ^{-1} is not unique. Instead of the Lagrange type interpolation polynomial, any other approximation formula of a function through intermediate values can be used.

4 Applications

In order to determine the functional characteristics and the performances of an actuator, the classical control method consisted in measuring directly these characteristics and performances with the help of transducers mounted onto the actuator undergoing the test. As it can be easily noticed, this method is disadvantageous for a real time control.

In order to overcome this situation, the novel proposed method of indirect measuring the performance of actuators was given in [1,2,3]. Supposing that the technical performances of the actuators we are about to test are expressed through a set of n standards or functioning specifications, in accordance to the new control method, verifying these parameters is not done directly, but through a reference actuator to which the trial actuators are connected, one at a time. In order to distinguish between the working parameters of the tested actuators and the response values of the functioning parameters of the reference actuator, to which these will be connected, we agree to denote by p_1, \dots, p_n the working parameters of the trial actuators and by r_1, \dots, r_n the working parameters of the reference actuator. With these preparations, a mathematical approach for the novel proposed method is to consider it an "input-output system", like (1). It

should be noted that, except for the parameter q which is part of the input data (p_1, \dots, p_n, q) , the values of the other parameters p_1, \dots, p_n are not known explicitly, as they interact with the system Σ through the trial actuator which they describe implicitly. In this context, the mathematical model we have built has the role of converting the numerical values of the system outputs Σ : $(r_1(q), \dots, r_n(q))$, into the numerical values $(p_1(q), \dots, p_n(q))$, of the trial actuator parameters.

The presented method has the advantage of ensuring a decrease in the trials' duration and the realization of complex trial regimes.

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