

## Design and Development of simple low cost Rectangular Microstrip Antenna for multiband operation.

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**Abstract-** This paper presents the design and development of simple low cost rectangular microstrip antenna for multiband operation. By incorporating U-slot of optimum geometry and open stubs at two opposite corners on the rectangular radiating patch the antenna operates between 1.815 to 9.01 GHz at different frequency bands with a virtual size reduction of 44.84% and gives broadside radiation characteristics at each operating band. By placing U-slot and open stubs at the corners, the copper area of the patch is reduced to 8.50%, when compared to the copper area of conventional rectangular microstrip antenna designed for the same frequency. The experimental and simulated results are in good agreement with each other. The design concept of antenna is given and experimental results are discussed. The proposed antenna may find applications in mobile, WLAN, WiMax and SAR.

**Key words :** Open stubs, U-slot, multiband.

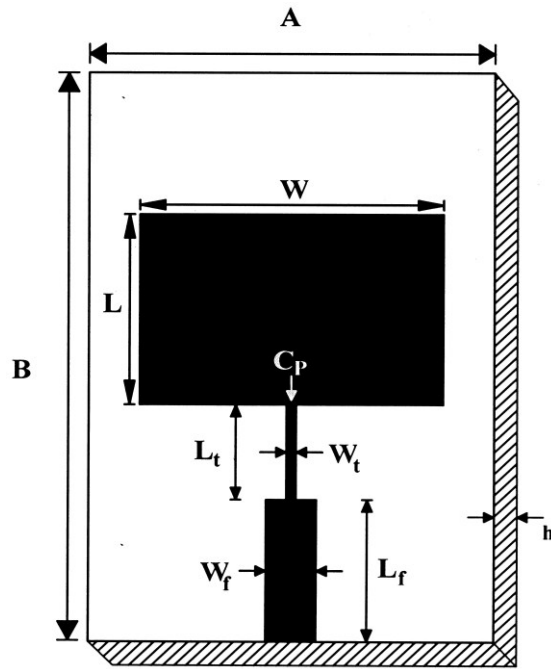
### 1. INTRODUCTION

In the present communication scenario microstrip antennas are becoming popular because of their numerous advantages like low profile, low fabrication cost, mechanical robustness, conformability to curved surfaces and integrability with MMICs [1]. Modern communication systems such as mobile, WLAN, WiMax and SAR are uses antennas operating at definite frequency bands. But a antenna operating at different frequency bands simultaneously is more useful and avoids the use of multiple antennas. The multiband antennas are realized by using many methods such as, variable inductive or capacitive loads to the patch [2], loading of shorting walls at different locations [3-4], stub loading technique [5], integrating varactor diodes to the radiating patches and changing their biasing voltages [6] etc. But in this study a simple technique has been used by loading U-slot and placing open stubs at the corners of the patch for multiband operation. This kind of study is found to be rare in the literature.

### 2. ANTENNA DESIGN

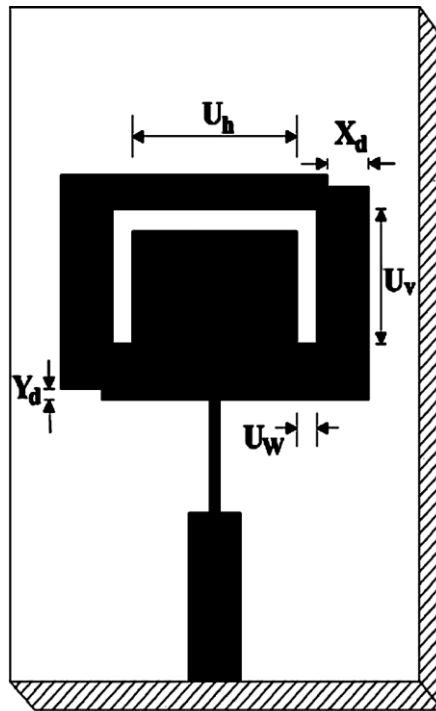
The conventional rectangular microstrip antenna (CRMSA) and the proposed U-slot rectangular microstrip antenna (USRMSA) are fabricated on low cost glass epoxy substrate material of thickness  $h = 0.166$  cm, loss tangent = 0.01 and  $\epsilon_r = 4.2$ . The art

work of proposed antennas is sketched using the computer software AUTO CAD to achieve better accuracy. The antennas are etched using the photolithography process.



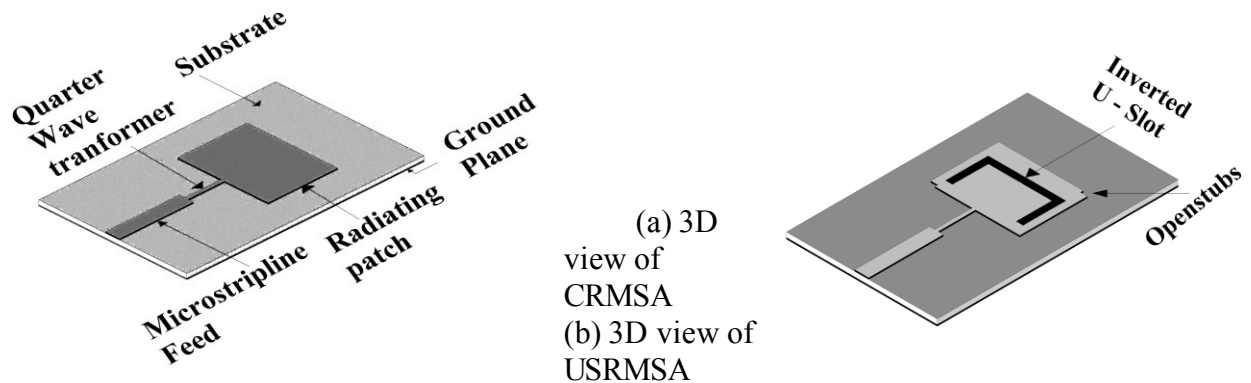
**Figure 1 Top view geometry of CRMSA.**

Figure 1 shows the top view geometry of CRMSA. The radiating patch of length  $L$  and width  $W$  are designed for the resonant frequency of 3.5 GHz, using the basic equations available in the literature [7]. A quarter wave transformer of length  $L_t$  and width  $W_t$  is used between  $C_p$  along the width of the patch and microstripline feed of length  $L_f$  and width  $W_f$  for matching their impedances.



**Figure 2 Top view geometry of USRMSA**

Figure 2 shows the top view geometry of USRMSA. This antenna is developed by placing open stubs at two diagonally opposite corners of CRMSA with the dimensions of  $X_d$  and  $Y_d$ . The U-slot is placed symmetrical about the center on the patch. The horizontal arm length  $U_h$  and the vertical arm length  $U_v$  of U-slot are taken as  $\lambda_0/6$ , where  $\lambda_0$  is the free space wavelength in cm corresponding to the designed frequency of 3.5 GHz. The  $U_w$  is the width of the horizontal and vertical arms of U-slot. Figure 3 (a) and (b) show the three dimensional view of CRMSA and USRMSA respectively. Table-1 shows the designed parameters of proposed antennas.



**Figure 3 3D views of CRMSA and USRMSA**

**Table 1. Design Parameters of proposed antennas**

Antenna Parameters	W	W <sub>f</sub>	W <sub>t</sub>	L	L <sub>f</sub>	L <sub>t</sub>	U <sub>h</sub>	U <sub>v</sub>	X <sub>d</sub>	Y <sub>d</sub>	A	B
Dimensions in cm	2.66	0.32	0.06	2.04	2.18	1.09	$\lambda_0/85$	$\lambda_0/42$	0.8	0.2	5	8

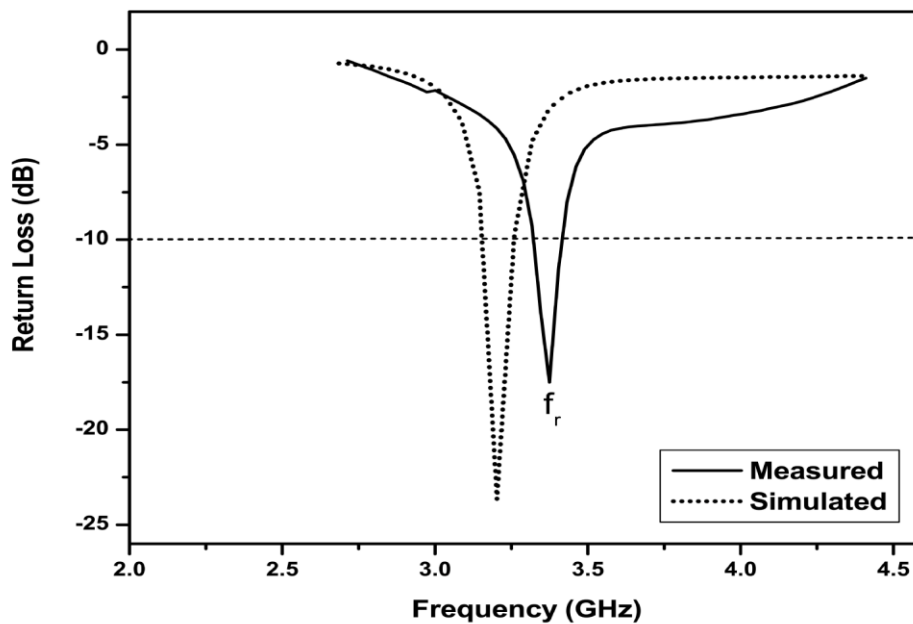
### 3. RESULTS AND DISCUSSION

The German make (Rohde and Schwarz, ZVK model 1127.8651) Vector Network Analyzer is used to measure the experimental return loss of CRMSA and USRMSA. The simulation of the CRMSA and USRMSA is carried out by using Ansoft HFSS simulation software.

Figure 4 shows the variation of return loss versus frequency of CRMSA. From this figure it is seen that, the CRMSA resonates at 3.39 GHz of frequency which is close to the designed frequency of 3.5 GHz. The experimental bandwidth is calculated using the formula,

$$\text{Bandwidth (\%)} = \frac{f_2 - f_1}{f_c} \times 100\%$$

where,  $f_2$  and  $f_1$  are the upper and lower cut off frequencies of the resonated band when its return loss reaches -10dB and  $f_c$  is a centre frequency between  $f_1$  and  $f_2$ . The bandwidth of CRMSA is found to be 3.27 %. The simulated result of CRMSA is also shown in Fig. 4.



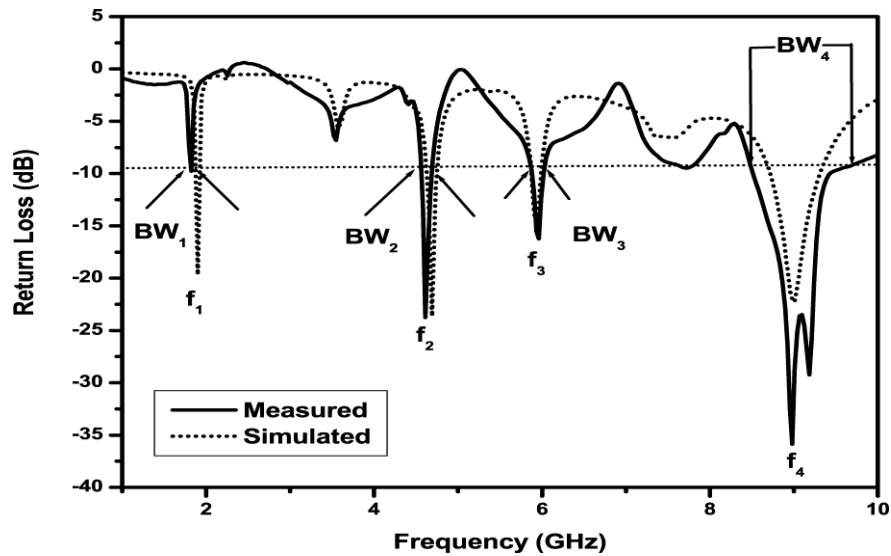
**Figure 4** Variation of return loss versus frequency of CRMSA**Figure 5** Variation of return loss versus frequency of USRMSA when  $U_w = 0.1$  cm

Figure 5 shows the variation of return loss versus frequency of USRMSA. It is clear from this figure that, the antenna operates for four bands  $BW_1$  (1.779-1.851 GHz),  $BW_2$  (4.53-4.72 GHz),  $BW_3$  (5.83-6.1 GHz) and  $BW_4$  (8.44-9.75 GHz) for the resonating modes of  $f_1$ ,  $f_2$ ,  $f_3$  and  $f_4$  respectively, when  $U_w = 0.1$  cm. The four bands  $BW_1$ ,  $BW_2$ ,  $BW_3$  and  $BW_4$  are due to the independent resonance of patch, two open stubs and U-slot of USRMSA respectively. The simulated result of USRMSA is also shown in Fig. 5 which is in good agreement with the experimental results. The magnitude of operating bandwidth  $BW_1$ ,  $BW_2$ ,  $BW_3$  and  $BW_4$  are found to be 3.96 %, 4.11 %, 4.525 % and 14.4% respectively. By comparing the resonant mode  $f_1$  of USRMSA to  $f_r$  of CRMSA it is clear that, the USRMSA gives virtual size reduction of 44.84%. Further USRMSA uses less copper area of 8.50% when compared to the copper area of CRMSA by placing U-slot and open stubs on the patch.

The far field co-polar and cross-polar radiation patterns of the proposed antennas are measured in their operating bands. The typical radiation patterns of CRMSA and USRMSA measured at 3.39 and 4.62 GHz are as shown in Fig. 6 and 7 respectively.

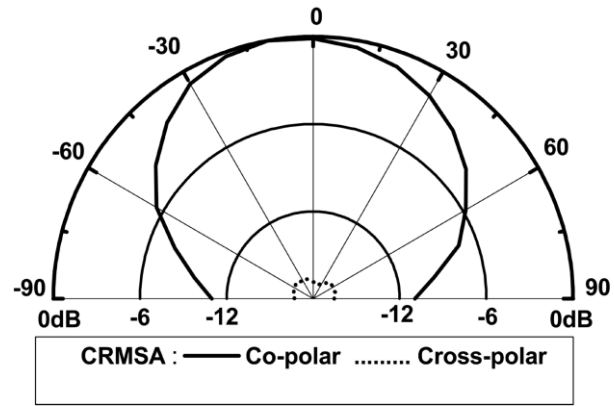


Figure 6 Radiation pattern CRMSA measured at 3.39 GHz

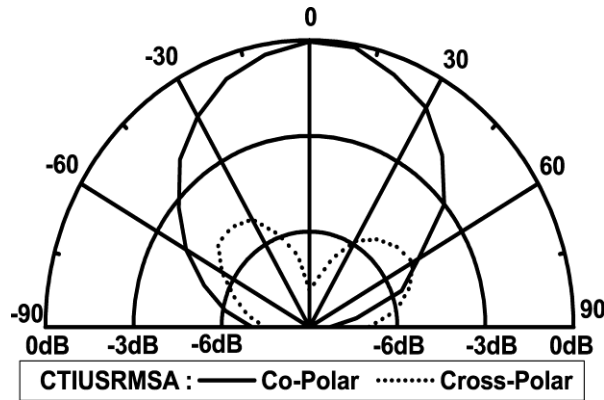


Figure 7 Radiation pattern of USRMSA measured at 4.62 GHz

From these figures it is observed that, the patterns are broadsided and linearly polarized. The gain in dB of antenna under test (AUT) is calculated using absolute gain method given by the equation [14],

$$G \text{ (dB)} = 10 \log\left(\frac{P_r}{P_t}\right) - (G_t) \text{ dB} - 20 \log\left(\frac{\lambda_0}{4\pi R}\right) \text{ dB}$$

where,  $P_t$  and  $P_r$  are transmitted and received powers respectively.  $R$  is the distance between transmitting antenna and AUT. The peak gain USRMSA measured in  $BW_1$  is found to be 0.60dB.

#### 4. Conclusion

From the detailed study it is clear that, multiband operation of antenna can be achieved through the novel design of USRMSA which is constructed from CRMSA. The antenna operates between 1.815 to 9.01 GHz at different frequency bands with a virtual size reduction of 44.84% and gives broadside radiation characteristics at each operating band.

By placing U-slot and open stubs at the corners, the copper area of the patch is reduced to 8.50%, when compared to the copper area of conventional rectangular microstrip antenna. The experimental results of return loss versus frequency of proposed antennas are in good agreement with the simulated results. The proposed antennas are simple in their design and fabrication and they use low cost substrate material. These antennas may find applications in mobile communication, wireless local area network (WLAN), worldwide interoperability for microwave access (WiMAX) and synthetic aperture radar (SAR).

### **Acknowledgement**

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